frequency shift (important for next generation) electric dipole moment searches ) induced in confined gases by a magnetic field gradient: Detailed discussion of a linear electric field Implications for electric dipole moment experiments (II)

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#### Abstract

The search for particle electric dipole moments represents a most promising way to search for physics beyond the standard model. A number of groups are planning a new generation of experiments using stored gases of various kinds. In order to achieve the target sensitivities it will be necessary to deal with the systematic error resulting from the interaction of the well-known  $\overrightarrow{v} \times \overrightarrow{E}$  field with magnetic field gradients (often referred to as the geometric phase effect [9], [10]. This interaction produces a frequency shift linear in the electric field, mimicking an edm. In this work we introduce an analytic model for the correlation function which determines the behavior of the frequency shift [11] and show in detail how it depends on the operating conditions of the experiment. We also propose a method to directly measure ths correlation function under the exact conditions of a given experiment.

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#### 1 Introduction

represent a broad range of operating conditions, from room temperature gases with buffer gas to laser cooled atoms in a MOT. reach sensitivities in the range of  $10^{-27}-10^{-28}e-cm$ . Sensitivity in this range several species of confined gases [4] including Radium [5], Radon [6] and Xenon a recent review). Experiments on several systems including the neutron [3] is inspiring many groups to search for edm's in a variety of systems. (See [2] for resents a reasonable method to look for physics beyond the standard model [1] The proposition that the search for particle electric dipole moments (edm) rephas already been achieved in the case of Hg [8]. The experiments proposed [7] are in various stages of preparation. These experiments are all hoping to

systematic effect, each of the proposed experiments will have to be analyzed operating conditions of the experiment. While experiments in small vessels and effect [9], [10] this interaction produces a frequency shift linear in the electric field, mimicking an edm. This systematic effect is highly dependent on the field with magnetic field gradients. Often referred to as the geometric phase the systematic error resulting from the interaction of the well-known  $\overrightarrow{v}$ with high pressure buffer gas are expected to be relatively insensitive to the In order to achieve the target sensitivities it will be necessary to deal with  $\times$ 

how it depends on the operating conditions of the experiment. For clarity we specialize the discussion to to the Los Alamos proposal for a neutron edm search a co-magnetometer, [12] but the generalization to other cases is straightforward. using Ultra-cold neutrons (UCN) and  $He^3$  atoms diffusing in superfluid  $He^4$  as which determines the behavior of the frequency shift [11] and show in detail with it. In this work we introduce an analytic form of the correlation function in detail to judge its sensitivity to the effect and to find methods of dealing

connection with experiments involving stored particle gases. Additional discus-First analyzed by Commins [9] in the context of a beam experiment, the frequency shift has been discussed in some detail by Pendlebury et al [10] in

mean free path and wall specularity. which appeared as figure 3 in [11]. This is a plot of the normalized (linear in E) sion and calculations have been given by [11].

Our present understanding of the effect can best be summarized by figure 1, frequency shift vs. normalized Larmor frequency for various values of collision

[[11], equ 26] the frequency shift is given by velocity correlation function and taking the Fourier transform. According to These results have been obtained by numerical simulation of the position-

$$\delta\omega = ab \lim_{t \to \infty} \int_0^t d\tau R(\tau) \cos \omega_o \tau \tag{1}$$

where  $R(\tau)$  is the position velocity correlation function defined in [[11], equ.

$$R(\tau) = \langle \overrightarrow{r}(t) \cdot \overrightarrow{v}(t-\tau) - \overrightarrow{r}(t-\tau) \cdot \overrightarrow{v}(t) \rangle$$
 (2)

appealing to try to make use of the zero crossing, apparent in figure 1, to reduce and  $a = \frac{\gamma}{2} \partial B_z / \partial z$ ,  $b = \gamma E/c$ . From the experimental point of view it is very

spectrum of the correlation function, i.e. the frequency dependence of the shift, the zero crossing, considerably. We also propose a method for measuring the compared to the vessel size, we calculate the temperature dependence of the frequency shift for  ${}^3He$  diffusing in superfluid  ${}^4He$ . This is an experimentally and compare it to the results obtained previously by numerical simulations favored regime as collisions are seen to reduce the effect, as well as the slope at Using the limiting form of this model, valid for collision mean free paths small In this note we present an analytic model for the correlation function  $R\left( au
ight)$ 

### N Analytical model for the correlation function

#### 2.1 Gas collisions

average time between collisions the velocity autocorrelation function will have 1) We consider a particle that moves among scattering centers. If  $\tau_c$  is the

the form [14]

$$\psi(t) \equiv \langle \vec{v}(t)\vec{v}(0)\rangle = v^2 e^{-\frac{\tau}{\tau_c}}.$$
 (3)

In the other words,  $\psi(t)$  obeys the equation:

$$\frac{d\psi(t)}{dt} + \frac{1}{\tau_c}\psi(t) = 0. \tag{4}$$

#### 2.2 Wall collisions

We consider particles moving in a cylindrical storage cell in a vacuum. As shown in [10],[11] the frequency shift depends only on the motion in the x,y plane. Referring to figure 2, the trajectory sweeps out an angle

$$\alpha = \arccos\left(r/R\right)$$

with respect to the center in a time

$$\frac{\tau_{wall}}{2} = \frac{\sqrt{R^2 - r^2}}{v}$$

where  $\tau_{wall}$  is the time between wall collisions. The average angular velocity for a single trajectory is then

$$\omega = \frac{\arccos(r/R) v}{\sqrt{R^2 - r^2}}.$$

The average squared frequency for all particles with velocity v (in the x,y plane) has been given by [10], equ. (28) as

$$\langle \omega_o^2 \rangle = \frac{\pi^2}{6} \left( \frac{v^2}{R^2} \right) \tag{5}$$

but the mean square of the fundamental frequency will be given by (5). As the motion is not strictly circular each trajectory will experience a complicated spectrum for the time varying field (Ref. [10], section IV D and figure 7),

Assuming that the result is dominated by the fundamental frequency, the velocity autocorrelation function will, to this approximation, obey the equation:

$$\frac{d^2\psi(t)}{dt^2} + \langle \omega_o^2 \rangle \, \psi(t) = 0, \tag{6}$$

## 2.2.1 Non-specular wall collisions

a phase change harmonic oscillator. During one traversal of the cell the oscillator will undergo Following the proceeding section we are modelling the correlation function as a

$$\phi = \omega \tau_{wall} = 2\alpha = 2\arccos(r/R)$$

the accumulated oscillator phase by angle for the next collision,  $\chi$ , by a random amount  $\Delta \chi$  and hence a change in A non-specular reflection from the wall would result in a change in the incident

$$\Delta \phi = \frac{d\phi}{d\chi} \Delta \chi$$
$$\frac{d\phi}{d\chi} = \frac{d\phi}{dr} \frac{dr}{d\chi}$$

With

$$\sin \chi = r/R$$
$$\cos \chi = \sqrt{1 - r^2/R^2}$$

we have

$$\frac{d\chi}{dr} = \frac{1}{\sqrt{R^2 - r^2}}$$
$$\frac{d\phi}{dr} = \frac{2}{R\sqrt{1 - r^2/R^2}}$$

S

$$\Delta \phi = 2\Delta \chi$$

Since the changes  $\Delta \phi$  are random the phase  $\phi$  will make a random walk so that after a time t we will have

$$\left\langle \left(\Delta\phi\right)^{2}\right\rangle _{t}=4\left\langle \left(\Delta\chi\right)^{2}\right\rangle \frac{t}{\tau_{wall}}=2\left\langle \left(\Delta\chi\right)^{2}\right\rangle \frac{tv}{\sqrt{R^{2}-r^{2}}}$$

Averaging the amplitude of the oscillator over the distribution of  $\Delta\phi$  the amplitude will be reduced by

$$\langle \cos \phi \rangle = 1 - \frac{1}{2} \left\langle (\Delta \phi)^2 \right\rangle_t \equiv 1 - \frac{t}{\tau_{non-spec}} \sim \exp\left(-\frac{t}{\tau_{non-spec}}\right)$$

Thus we have

$$\frac{1}{\tau_{non-spec}} = \frac{\left\langle \left(\Delta \chi\right)^2 \right\rangle v}{\sqrt{R^2 - r^2}}.$$

Averaging over r we find

$$\left\langle \frac{1}{\tau_{non-spec}} \right\rangle = \left\langle \left( \Delta \chi \right)^2 \right\rangle v \int_0^R \frac{F\left(r\right) dr}{\sqrt{R^2 - r^2}} = \frac{4}{\pi} \left\langle \left( \Delta \chi \right)^2 \right\rangle \frac{v}{R},$$

where F(r) dr is the probability that a trajectory has a pericentric distance between r, r+dr:

$$F\left(r\right) = \frac{4\sqrt{R^2 - r^2}}{\pi R^2}.$$

# Model expression for the correlation function

When the particles are moving inside a vessel containing scatterers, one can expect that the equation for the velocity correlation function is the combination of (4) and (6), thus we are led to write

$$\frac{d^2\psi(\tau)}{d\tau^2} + \frac{1}{\tau_c} \frac{d\psi(\tau)}{d\tau} + \left\langle \omega_0^2 \right\rangle \psi(\tau) = 0. \tag{7}$$

This is just the equation for a damped harmonic oscillator and its general solution is of the form:

$$\psi(\tau) = c_1 e^{-\eta_1 \tau} + c_2 e^{-\eta_2 \tau}, \tag{8}$$

$$\eta_1 = \frac{1}{2\tau_c} + \sqrt{\frac{1}{4\tau_c^2} - \langle \omega_0^2 \rangle}, \qquad \eta_2 = \frac{1}{2\tau_c} - \sqrt{\frac{1}{4\tau_c^2} - \langle \omega_0^2 \rangle}.$$
Then, we have for the boundary condition satisfied by  $\psi(\tau)$ , [11]

$$h(\tau) = \int_{0}^{\tau} \psi(t)dt = \frac{R(\tau)}{2} \to 0, \quad \text{when} \quad \tau \to \infty.$$

Thus, the velocity correlation function  $[\psi(\tau)=\langle \vec{v}(t)\vec{v}(0)\rangle]$  will have the form:

$$\psi(\tau) = \frac{\eta_1 v^2}{\eta_1 - \eta_2} \left( e^{-\eta_1 \tau} - \frac{\eta_2}{\eta_1} e^{-\eta_2 \tau} \right). \tag{10}$$
 and the function  $R(\tau)$  will be given by:

$$R(\tau) = 2 \int_{0}^{\tau} \psi(x) dx = \frac{2v^{2}}{\eta_{1} - \eta_{2}} \left( 1 - e^{-(\eta_{1} - \eta_{2})\tau} \right) e^{-\eta_{2}\tau}. \tag{11}$$

## 2.3.1 Overdamped, short mean free path, limit

In the overdamped limit

$$\frac{1}{2\tau_c} \gg \omega_0 \tag{12}$$

we find:

$$\eta_1 \simeq \frac{1}{\tau_c}, \qquad \eta_2 \simeq \tau_c \left\langle \omega_0^2 \right\rangle, \qquad \eta_1 \gg \eta_2.$$
(13)

Therefore:

$$R(\tau) = 2\lambda v \left(1 - e^{-\frac{\tau}{\tau_c}}\right) e^{-\frac{\tau}{T}},\tag{14}$$

$$T = \frac{1}{\tau_c \langle \omega_0^2 \rangle} = \left(\frac{6}{\pi^2}\right) \frac{R^2}{v\lambda}.$$
 (15)

using (5).

[11] (for a cylinder), were seen to be in good agreement (in the short mean free path limit) with equ. (14) above (equation 43, [11]) with The numerical simulations of the correlation function shown in figure 1 of

$$T = .6R^2/\lambda v \tag{16}$$

where  $\lambda$  is the collision mean free path, v is the particle velocity and R is the radius of the cylindrical measurement cell, (taken as R=25, in the rest of this paper). The factor 0.6 in equation (16) is in good agreement with the factor = 0.608) in equation (15).

temperature For UCN on the other hand the only collisions are those with the walls, all parameters are independent of temperature and we have to take the In the case of  $He^3$  moving in superfluid  $He^4$ ,  $\tau_c$ , v and  $\lambda$  are all functions of

$$\frac{1}{2\tau_c} \ll \omega_0.$$

path limit (14), green. numerical simulation, red, the model equ. (11), blue and the short mean free In figure 3 we show a comparison of the correlation functions calculated by

in our model of higher harmonics of the motional frequency range of  $r_o$  and the short mean free path expression (14), (green), is a reasonable fit for  $r_o \gtrsim 2.5$ . The disagreement for smaller  $r_o$  is most likely due to the neglect In the figures  $r_0 = R/\lambda$ . We see the model gives a reasonable fit for a wide

 $^3He$  diffusing in  $^4He$ , taking into account the velocity dependence of the mean over a Maxwell-Boltzman velocity distribution as a function of temperature for In the following we will use (14) to calculate the frequency shift averaged

### induced systematic Calculation of the zero crossing frequency for the $\mathbf{v} \times E$

transform of  $R(\tau)$  which is given by (2). For  $\exp(-\alpha |\tau|)$  the cosine Fourier transform is  $\alpha/(\alpha^2 + \omega^2)$  so that we have, using the short mean free path limit of the model, equation (14) According to (1) the frequency shift is proportional to  $S(\omega)$ , the cosine Fourier

$$S(\omega) = \left[ \frac{\eta_2}{\omega^2 + \eta_2^2} - \frac{\eta_1 + \eta_2}{\omega^2 + (\eta_1 + \eta_2)^2} \right] \lambda v \tag{17}$$

This is easily seen to have the correct limits for  $\omega \to 0, \infty$ , (equations 54 and 70 in [11]). To find the value of  $\omega$  where the effect goes to zero we put

$$S(\omega) = 0$$

$$\omega^{2} + (\eta_{1} + \eta_{2})^{2} = (\omega^{2} + \eta_{2}^{2}) \frac{(\eta_{1} + \eta_{2})}{\eta_{2}}$$

$$\omega = \sqrt{\eta_{1}\eta_{2} + \eta_{2}^{2}} \approx \sqrt{\eta_{1}\eta_{2}}$$

the limit, is at in the case where  $\eta_1 \gg \eta_2$  $(\lambda \ll R)$ . Thus we see that the zero crossing, in

$$\omega_o \approx \sqrt{\eta_1 \eta_2} = \sqrt{\frac{\lambda v}{.6 R^2 \tau_c}} = 1.3 \frac{v}{R}$$

which should hold for reasonably small values of  $\lambda/R$ . Thus for short  $\lambda$  all curves should have the same zero crossing. This is seen to be satisfied by the numerical simulations of figure 1.

### ಬ Frequency shift averaged over velocity distri-

realistic case (2) of a mean free path proportional to velocity in order to show do this for the case (1) of a constant collision man free path and then for the the influence of a variable collision mean free path. Fourier transform we can perform an average over the velocity distribution. We Using the limiting analytical model (14) for the correlation function and its

## Mean free path independent of velocity

The frequency shift, is given in terms of the spectrum  $S(\omega)$  (17) by:

$$\delta\omega(\omega,T) = abS(\omega)$$

$$\delta\omega(\omega, T) = abR^{2}(.6) \left[ \frac{(k(T)/.6)^{2}}{(\omega R/v)^{2} + (k(T)/.6)^{2}} - \frac{(k(T)/.6)(k(T)/.6 + 1/k(T))^{2}}{(\omega R/v)^{2} + (k(T)/.6 + 1/k(T))^{2}} \right]$$

with  $k = \lambda/R = 1/r_o$  being a function of temperature  $(\lambda(T) = 3D(T)/v(T))$  as shown in figure 3c),  $(D(T) = 1.6/T^7)$  is the diffusion coefficient for  $He^3$  in  $He^4$  as measured by [13], and we have taken R = 25).

The average of this over the velocity distribution of the  $He^3$  will be given

$$\langle \delta\omega(\omega,T) \rangle = \frac{4}{\sqrt{\pi}} \int \delta\omega(\omega,T) \frac{v^2}{\beta^2} e^{-v^2/\beta^2} \frac{dv}{\beta}$$

$$= abR^2 (.6) \frac{4}{\sqrt{\pi}} \int_0^\infty \left[ \frac{1}{(\omega R/\alpha_2)^2 + v^2} - \frac{\alpha_2/\alpha_1}{(\omega R/\alpha_1)^2 + v^2} \right] v^4 e^{-v^2/\beta^2} \frac{dv}{\beta^3}$$
where  $C = \frac{(L(T)/\mathcal{E})}{2} = \frac$ 

where  $\alpha_2 = (k(T)/.6)$ ,  $\alpha_1 = (k(T)/.6 + 1/k(T))$ . Now we have

$$\frac{4}{\sqrt{\pi}} \int_0^\infty \frac{x^4}{a^2 + x^2} e^{-x^2/\beta^2} dx \equiv F(a, \beta) = 2a^3 \sqrt{\pi} e^{\frac{a^2}{\beta^2}} \left( 1 - \operatorname{erf}\left(\frac{a}{\beta}\right) \right) - 2a^2 \beta + \beta^3$$
(19)

$$\begin{split} \langle \delta\omega(\omega,T) \rangle &= \frac{abR^2}{\beta^3} \left(.6\right) \left[ F\left(\frac{\omega R}{\alpha_2},\beta(T)\right) - \frac{\alpha_2}{\alpha_1} F\left(\frac{\omega R}{\alpha_1},\beta(T)\right) \right] \\ &\equiv abR^2\Omega\left(\omega,T\right) \end{split}$$

 $He^4$ .  $F(a,\beta)$  tends to be difficult to calculate numerically for  $\alpha/\beta \gtrsim 5$  so we will use the asymptotic expansion (Ref. [15], section 7.1.23, pg 298) where  $\beta(T) = 1.28 \times 10^4 \sqrt{\frac{7}{7.2}} cm/\text{sec}$  is the most probable velocity for  $He^3$  in

$$\sqrt{\pi}e^{z^2}\operatorname{erf} c(z) \to \left(\frac{1}{z}\right)\left(1 - \frac{1}{2z^2} + \frac{3}{4z^4} - \frac{15}{8z^6} + \dots\right)$$

for  $\alpha/\beta > 4$ . Note that the leading term in the expansion is canceled by the term  $2a^2\beta$  in (19). To plot the results we choose

$$X(\omega, T) = \omega R/\beta(T) \tag{20}$$

as the independent variable.

able velocity, (20): quency shift plotted versus the frequency relative to the appropriate, most prob-Figure 4 shows the normalized, averaged over the velocity distribution, fre-

Expanding the plot we see the region near the zero crossing (figure 5) and expanding still further (figure 6)

smaller (increasing temperature) just as in the single velocity case (section 2.4). In this figure we see the zero crossings converging as the mean free path gets

plot the results as a function of temperature. From the point of view of an experiment it is perhaps more interesting to

quency shift for a range of frequencies specified by the corresponding values of  $X(\omega,T)$ , (equ. 20), i.e.  $\omega=\frac{\beta(T)}{R}X(\omega,T)$ . Expanding the plot (figure 8) shows the region where the effect can be min-Figure 7 shows the temperature dependence of the velocity averaged fre-

imized:

averaging does indeed reduce the effect. In fact reductions of  $10^{-5}$ appear feasible. Here we see that the applied frequency can be chosen so that the velocity

### ა. 2 Mean free path $\propto velocity$ , cross section $\sim 1/v$

move a distance  $\lambda_v(T) = v\tau_c(T)$ . Thus We have  $k(T) = \lambda(T)/R$ . Since the velocity of the  $He^3$  is much less than the phonon velocity  $(2.2 \times 10^4 cm/\text{sec})$  the collision rate of phonons with the  $He^3$  will be independent of the  $He^3$  velocity. In a time  $\tau_c$  a  $He^3$  with velocity v, will

$$k_v(T) = \lambda_v(T)/R = v\tau_c(T)/R = v/s(T)$$

with  $s(T) = R/\tau_c(T)$ . From equation (18)

$$\delta\omega(\omega, T) = abR^{2}(.6) \left[ \frac{(k_{v}(T)/.6)^{2}}{(\omega R/v)^{2} + (k_{v}(T)/.6)^{2}} - \frac{(k_{v}(T)/.6)(k_{v}(T)/.6 + 1/k_{v}(T))}{(\omega R/v)^{2} + (k_{v}(T)/.6 + 1/k_{v}(T))^{2}} \right]$$
(21)

The average of this over the velocity distribution of the  $He^3$  will be given by

$$\langle \delta\omega(\omega, T) \rangle = \frac{4}{\sqrt{\pi}} \int \delta\omega(\omega, T) \frac{v^2}{\beta^2} e^{-v^2/\beta^2} \frac{dv}{\beta}$$

$$= ab R^2 (.6) \frac{4}{\sqrt{\pi}} \int_0^\infty \left[ \frac{1}{(\omega R/\alpha_2)^2 + v^2} - \frac{\alpha_2/\alpha_1}{(\omega R/\alpha_1)^2 + v^2} \right] v^4 e^{-v^2/\beta^2} \frac{dv}{\beta^3}$$

$$\equiv ab R^2 \Psi(\omega, T) \tag{23}$$

where  $\alpha_2 = (k_v(T)/.6)$ ,  $\alpha_1 = (k_v(T)/.6 + 1/k_v(T))$ . In the region of interest for suppression of the effect,  $k_v(T) \ll 1$ , we have  $\alpha_1 \sim 1/k_v(T)$ . Then the integral in (22) can be written

$$= \int_0^\infty \left[ \frac{y^2}{\left(\frac{.6s}{\beta(T)}\right)^2 \left(\frac{\omega R}{\beta(T)}\right)^2 + y^4} - \frac{1/.6}{\left(\frac{\omega R}{\beta(T)}\right)^2 + \frac{s(T)^2}{\beta(T)^2}} \right] y^4 e^{-y^2} dy$$

where  $y = v/\beta(T)$ . The second integral can be evaluated as

$$\int_0^\infty y^4 e^{-y^2} dy = \frac{3}{2} \frac{\sqrt{\pi}}{4}$$

Defining

$$x(\omega, T) = \frac{\omega R}{\beta(T)}$$

and writing

$$\frac{s(T)}{\beta(T)} = \frac{R}{\beta(T)\tau_c(T)} = \frac{R}{\lambda_c(T)} = \frac{1}{k(T)}$$

where  $\lambda_c(T)$  and k(T) are evaluated at the most probable velocity  $\beta(T)$ , we have  $a(T) = \left(\frac{6s}{\beta(T)}\right) \left(\frac{\omega R}{\beta(T)}\right) = \frac{6}{k(T)}x(\omega, T)$ 

The first integral can be evaluated in terms of a hypergeometric function (hypergeom ([1],  $\begin{bmatrix} \frac{1}{4}, -\frac{1}{4} \end{bmatrix}, -\frac{1}{4}x^2$ )) but the series for this has some convergence difficulties for the parameters of interest. Thus we define

$$f(a) = \int_0^\infty \frac{y^6}{a^2 + y^4} e^{-y^2} dy$$

(to be evaluated numerically as the integrand is well behaved) so that

$$\Psi\left(\omega,T\right) = (.6) \left[ \frac{4}{\sqrt{\pi}} f\left[ \frac{.6}{k(T)} x(\omega,T) \right] - \frac{2.5}{\left(x(\omega,T)\right)^2 + \left(\frac{1}{k(T)}\right)^2} \right]$$
(24)

dence of the mean free path. In figure 9 we plot the frequency shift averaged over velocity as a function of Larmor frequency for fixed temperature taking into account the velocity dependence.

Figures 10 and 11 show the frequency shift as a function of temperature for

# Measurement of the correlation function, $R(\tau)$

measure the frequency spectrum of the relevant correlation function (2) and In this section we present a generally applicable, straightforward method to hence the frequency dependence of the frequency shift directly. it experimentally and to check its applicability to other edm searches in progress. While the theory presented here is expected to be accurate for the case of polarized  $He^3$  diffusing in superfluid  $He^4$  it would be nice to be able to confirm

field in the x-y plane  $\overrightarrow{B}_{\overrightarrow{r}}=-\left(\overrightarrow{r}/2\right)\left(\partial B_{z}/\partial z\right).$  Then If we apply a uniform magnetic field gradient  $\partial B_z/\partial z$  large enough so that it dominates all other field gradients that may be present, there will be a radial

$$\frac{\partial B_{x,y}}{\partial x, y} = -\frac{1}{2} \frac{\partial B_z}{\partial z} = -a$$

and the field correlation functions will be

$$\langle B_{x_i}(t) B_{x_i}(t+\tau) \rangle = (a)^2 \langle x_i(t) x_i(t+\tau) \rangle$$

where  $x_i = x$  or y. Then following McGregor [14] the relaxation time,  $T_1$  will be given by (in the case when  $\partial B_z/\partial z$  is large enough so that wall relaxation can be neglected)

$$\frac{1}{T_1} = \frac{\gamma^2 a^2}{2} \left[ S_r \left( \omega_o \right) \right]$$

₩.h

$$S_{r}(\omega) = \int_{-\infty}^{\infty} \langle \overrightarrow{r} \underline{\uparrow}(t) \cdot \overrightarrow{r} \underline{\uparrow}(t+\tau) \rangle e^{-i\omega\tau} d\tau$$
$$= \int_{-\infty}^{\infty} R_{\overrightarrow{\tau}} \underline{\uparrow}(\tau) \cos \omega \tau d\tau$$

where we recognize that the correlation function  $R_{\overrightarrow{r}} \neq (\tau)$  is an even function of  $\tau$ . A measurement of  $T_1$  will thus yield the function  $S_r(\omega)$ . Now

$$\omega^{2} S_{r} (\omega) = -\int_{-\infty}^{\infty} R_{\overrightarrow{r}} \overrightarrow{r} (\tau) \frac{d^{2}}{d\tau^{2}} (\cos \omega \tau) d\tau$$
$$= -\int_{-\infty}^{\infty} \frac{d^{2} R_{\overrightarrow{r}} \overrightarrow{r} (\tau)}{d\tau^{2}} (\cos \omega \tau) d\tau$$
$$= \int_{-\infty}^{\infty} R_{\overrightarrow{r}} \overrightarrow{r} (\tau) (\cos \omega \tau) d\tau$$

function. Then where we used  $R_{\overrightarrow{v}} \overrightarrow{v}(\tau) = -d^2 R_{\overrightarrow{r}} \overrightarrow{r}(\tau)/d\tau^2$  [16] for the velocity correlation

$$R_{\overrightarrow{v}}_{\overrightarrow{v}}(\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \omega^2 S_r(\omega) \cos \omega \tau d\tau$$

By comparison with equ (38) of [11] we identify  $\omega^2 S_r(\omega)/2\pi$  with  $\psi(\omega)$  of that work and we then see that the systematic frequency shift is given by (equation

$$\delta\omega = -\frac{ab}{2\pi} \int_{-\infty}^{\infty} \frac{\omega^2 S_r(\omega)}{(\omega_o^2 - \omega^2)} d\omega$$
 (25)

Since we can determine  $S_r(\omega)$  from the  $T_1$  measurements we can determine the frequency dependence of the systematic frequency shift for any experimental conditions without the need of applying an electric field.

# 5 Arbitrary Magnetic field geometry

low frequency (diffusion) limit. In this section we discuss this problem using our recent note, Harris and Pendlebury [17] have shown that in the case of a field average of  $G_z$  in the high frequency (called by them the adiabatic) limit. In a that regardless of the field geometry the effect only depends on the volume constant. Pendlebury et al [10] have shown, using a geometric phase argument, is happening and display details of the transition from one case to another. correlation function approach in order to give some physical insight into what produced by a dipole external to the measurement cell, this does not hold in the Our discussion has assumed a magnetic field configuration with  $G_z = \partial B_z/\partial z$ 

### Short time (high frequency, adiabatic) limit of the correlation function

by the neutrons as they move through the apparatus. Equation (23) of that paper gives the frequency shift proportional to E as  $(\overrightarrow{\omega}(t))$  lies in the x, y plane) Reference [11], has shown that the systematic edm is given, in general, as the Fourier transform of a certain correlation function of the time varying field seen

$$\delta\omega_{E}(t) = -\frac{1}{2} \int_{0}^{t} d\tau \left\{ -\sin\omega_{o}\tau \left[\overrightarrow{\omega}_{x}(t) \times \overrightarrow{\omega}_{x}(t-\tau)\right] + \omega_{y}(t-\tau)\omega_{y}(t) \right] \right\}$$
(26)

It can be shown that the term multiplying  $\sin \omega_o \tau$  goes to zero on averaging over a uniform velocity distribution  $(\langle v_x v_y \rangle = 0, \quad v_x^2 = v_y^2 = v^2/2)$  and using  $\overrightarrow{\nabla} \times \overrightarrow{B} = 0$ . Then, for short times,  $\tau$ ,

$$\delta\omega(t) = -\frac{1}{2} \int_0^t d\tau \left\{ \cos\omega_o \tau \left[ \overrightarrow{\omega}(t) \times \left( \overrightarrow{\omega}(t) - \frac{d\overrightarrow{\omega}}{dt} \tau + \frac{1}{2} \frac{d^2 \overrightarrow{\omega}}{d\tau^2} \tau^2 + \dots \right) \right] \right\}$$

$$= -\frac{1}{2} \int_0^t d\tau \left\{ \cos\omega_o \tau \left[ -\overrightarrow{\omega}(t) \times \left( \frac{d\overrightarrow{\omega}}{dt} \tau - \frac{1}{2} \frac{d^2 \overrightarrow{\omega}}{d\tau^2} \tau^2 + \dots \right) \right] \right\}$$
(27)
We are considering values of  $\tau$  so small that the velocity doesn't change in that time interval  $(\tau < \tau_{coll})$ .

$$\overrightarrow{\omega}(t) = \gamma \left( \overrightarrow{B}_{xy}(t) + \overrightarrow{v}/c \times \overrightarrow{E} \right)$$

$$\frac{d\overrightarrow{\omega}}{dt} = \gamma \left( \overrightarrow{\nabla B} \left( \overrightarrow{x}(t) \right) \cdot \overrightarrow{v} \right)$$

$$\frac{d^2 \overrightarrow{\omega}}{d\tau^2} = \gamma \sum_{i,j} \frac{\partial^2 \overrightarrow{B}}{\partial x_i \partial x_j} v_i v_j$$

and
$$\delta\omega(t) = -\frac{\gamma}{2c} \int_0^t d\tau \cos \omega_o \tau \left[ -\left( \overrightarrow{B}_{xy}(t) + \overrightarrow{v} \times \overrightarrow{E} \right) \times \left( \frac{\partial \overrightarrow{\omega}}{\partial t} \tau - \frac{1}{2} \frac{\partial^2 \overrightarrow{\omega}}{\partial \tau^2} \tau^2 + \dots \right) \right]$$
(28)

The term linear in 
$$\overrightarrow{E}$$
 and  $\tau$  is then
$$\delta\omega(t) = -\frac{\gamma^2}{2c} \int_0^t d\tau \cos \omega_o \tau \left[ \left( \overrightarrow{\nabla B} \cdot \overrightarrow{v} \right) \tau \times \left( \overrightarrow{v} \times \overrightarrow{E} \right) \right]$$

$$\equiv \frac{\gamma E}{2} \int_0^t d\tau \cos \omega_o \tau \left( \alpha \tau \right)$$
(2)

$$\chi = \frac{\gamma}{c} \left( \overrightarrow{\nabla} \overrightarrow{B} \cdot \overrightarrow{v} \right) \cdot \overrightarrow{v}$$

We have now calculated the correlation function for short times. It starts at zero at  $\tau=0$  and rises as  $\alpha\tau$ . Eventually it will reach a maximum. By concentrating on the high frequency  $(\omega_o)$  behavior of  $\delta\omega$  the result will be independent of the details of the maximum, depending only on  $\alpha$ . Thus we can replace  $\alpha\tau$  in (29) by  $\sin\alpha\tau$  or any function with the same initial slope. Thus we are led to take

$$\delta\omega(t) \equiv \frac{\gamma E}{2} \lim_{\omega_o \to \infty} \int_0^t d\tau \cos \omega_o \tau \sin \alpha \tau$$
$$= \lim_{\omega_o \to \infty} \frac{\gamma E}{2} \frac{\alpha}{\omega_o^2 - \alpha^2} = \frac{\gamma E}{2} \frac{\alpha}{\omega_o^2}$$
$$= \frac{E}{2cB_o^2} \left( \overrightarrow{\nabla} \overrightarrow{B} \cdot \overrightarrow{v} \right) \cdot \overrightarrow{v}$$

Introducing components taking averages and using  $\overrightarrow{\nabla} \cdot \overrightarrow{B} = 0$  this reduces to

$$\overline{\delta\omega}_{geo} = -Ev^2 \frac{1}{4cB_o^2} \left\langle \frac{\partial B_z}{\partial z} \right\rangle \tag{30}$$

systematic (false) edm effect depends only on  $\langle \frac{\partial B_z}{\partial z} \rangle$  regardless of the geometry of the magnetic field, a result obtained previously by Pendlebury et al [10] and in agreement with equ. (2) of [11] if, in that equation,  $R^2\omega_r^2$  is replaced by  $\langle v^2 \rangle = v^2/2$ . We have shown that in the adiabatic (short time) limit the confirmed in [17].

The next order term in (28) is easily seen to be of order  $v^3\tau^2$  and so will average to zero, the next term which contributes will be of order  $v^4\tau^3$  and so will be negligible in the short time limit we are considering. The condition for this to be valid is  $(v\tau/\Lambda)^2 \ll 1$  where  $\Lambda$  is the scale of variations in the applied magnetic field  $\left(\frac{\partial B_z}{\partial z}\frac{1}{B_z} \sim \Lambda^{-1}\right)$ 

# Longer time behavior of the correlation function

For long times the expansion (27) is clearly not valid and we must expand in a series in the spatial coordinates. We start from

$$\delta\omega = -\frac{\gamma^2}{2} \int d\tau \cos\omega_o \tau \left\langle \overrightarrow{B}'(t) \times \overrightarrow{B}'(t-\tau) \right\rangle_z$$

where b = E/c, the brackets represent an ensemble average and

$$B'_{x} = B_{x} \left(\overrightarrow{r}\left(t\right)\right) - bv_{y}$$
  
$$B'_{y} = B_{y} \left(\overrightarrow{r}\left(t\right)\right) + bv_{x}$$

Then we write
$$\left\langle \overrightarrow{B}'(t) \times \overrightarrow{B}'(t-\tau) \right\rangle_{z} = b \left\langle \begin{array}{c} B_{x} \left(\overrightarrow{r}'(t)\right) v_{x} \left(t-\tau\right) - v_{y} \left(t\right) B_{y} \left(\overrightarrow{r}'(t-\tau)\right) \\ - \left(B_{x} \left(\overrightarrow{r}'(t-\tau)\right) v_{x} \left(t\right) - v_{y} \left(t\right) - v_{y} \left(t-\tau\right) B_{y} \left(\overrightarrow{r}'(t)\right) \right) \right\rangle \\ \end{array} (31)$$

and expand the field in a Taylor series

$$B_{x}\left(\overrightarrow{r}\left(t\right)\right) = \left(B_{x}\left(0,0,0,t\right) + \frac{\partial B_{x}}{\partial x} \middle|_{o} x\left(t\right) + \frac{\partial B_{x}}{\partial y} \middle|_{o} y\left(t\right) + \frac{\partial B_{x}}{\partial z} \middle|_{o} z\left(t\right)\right) + \left(\frac{\partial^{2} B_{x}}{\partial x^{2}} \middle|_{o} x^{2}\left(t\right) + \frac{\partial^{2} B_{x}}{\partial y^{2}} \middle|_{o} y^{2}\left(t\right) + \frac{\partial^{2} B_{x}}{\partial z^{2}} \middle|_{o} z^{2}\left(t\right)\right) + \left(\frac{\partial^{2} B_{x}}{\partial x \partial y} \middle|_{o} y\left(t\right) x\left(t\right) + \frac{\partial^{2} B_{x}}{\partial y \partial z} \middle|_{o} z\left(t\right) y\left(t\right) + \frac{\partial^{2} B_{x}}{\partial z \partial x} \middle|_{o} x\left(t\right) z\left(t\right)\right) + \left(\frac{\partial^{3} B_{x}}{\partial x^{3}} \middle|_{o} x^{3}\left(t\right) + \frac{\partial^{3} B_{x}}{\partial y^{3}} \middle|_{o} y^{3}\left(t\right) + \dots\right)$$

that there are no correlations between any functions  $f(x_i, v_i)$  and  $g(x_j, v_j)$  we (similarly for  $B_y$ ). Concentrating on the first and last terms in (31) and noting

$$\sum_{x_{i}=x,y}\left\langle \left(\left.\frac{\partial B_{x_{i}}}{\partial x_{i}}\right|_{o}x_{i}\left(t\right)+\frac{\partial^{2}B_{x_{i}}}{\partial x_{i}^{2}}\right|_{o}x_{i}^{2}\left(t\right)+\frac{\partial^{3}B_{x}}{\partial x_{i}^{3}}\right|_{o}x_{i}^{3}\left(t\right)...\right)v_{x_{i}}\left(t-\tau\right)-\left\{ \left(t\right)\Leftrightarrow\left(t-\tau\right)\right\} \right\rangle$$

where the second term is obtained from the first by interchanging (t) and  $(t-\tau)$ . By symmetry we see that  $\langle x_i^2(t) v_{x_i}(t-\tau) \rangle = 0$  so that the next contributing term will be proportional to

$$\frac{\partial^{3} B_{x}}{\partial x_{i}^{3}} \bigg|_{o} \left\langle x_{i}^{3} \left( t \right) v_{x_{i}} \left( t - \tau \right) \right\rangle$$

The first order term will be proportional to

$$\frac{\partial B_x}{\partial x} + \frac{\partial B_y}{\partial y} = -\frac{\partial B_z}{\partial z}$$

We see that the condition

$$\left. \frac{\partial^3 B_{x_i}}{\partial x_i^3} \right|_o R^2 \ll \left. \frac{\partial B_{x_i}}{\partial x_i} \right|_o \quad or \quad \frac{R^2}{\Lambda^2} \ll 1$$

our method cannot be applied since the higher order terms remain significant. will insure that the higher order terms can be neglected. In the extreme case considered by Harris and Pendlbury, [17], this condition is strongly violated so

#### Discussion

This shifts the effective frequency to higher values for the same value of reduced as seen from figure 1, and thus higher velocities contribute more to case (2). to zero, i.e reduced frequency  $\omega' \simeq 1.6$  in the case (1) of a constant mean free essentially unchanged. What is changed is the frequency where the effect goes We see that in both the case of a velocity independent mean free path and one proportional to velocity the behavior of the systematic frequency shift is This is because longer mean free paths contribute more to the frequency shift path and  $\omega' \simeq 2$  for the case (2) of a mean free path proportional to velocity.

and then average the result over the velocity distribution should be an excellent correlation function for an ensemble of trajectories with constant  $He^3$  velocity low  $He^3$  densities considered here. Thus our approach, where we calculate the phonon absorption is kinematically forbidden on a single  $He^3$  and can only take place as a result of  $He^3 - He^3$  collisions which will be negligible for the Due to the heavy mass and slow velocity of the  $He^3$ , Baym and Ebner [18] conclude that the phonon scattering on  $He^3$  is predominantly elastic. Single

effect to high degree. distribution of the  $He^3$  velocities, imply that one should be able to control the and figures 10 and 11, which are based on an exact average over the Maxwell fig.3 the limiting expression for the correlation function should be quite accurate Note that for temperatures  $T \gtrsim .38K$ ,  $r_o = 1/k \gtrsim 20$ , so that according to

which is represented by a point far to the right in figure 1). slightly negative i.e. equal in sign and magnitude with the shift for UCN. The UCN, with their relatively low value of  $\omega_r$  ( $\omega_o/\omega_r \gg 1$ ), have a frequency shift What would be ideal, would be to set the size of the shift for  $He^3$  to be

the temperature and magnetic field gradient stability. The limits on the ability to do this will be the usual experimental ones of

shift under the exact experimental conditions. allowing a precise determination of the frequency dependence of the frequency sible to measure the spectrum of the velocity correlation function directly, thus We have shown that by varying the gradients to larger values it will be pos-

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### 7 Figure Captions

is contained in the normalization of the frequency scale,  $\omega_r = v/R$ . Figure 1. Note the curves are for a single fixed velocity. The velocity dependence

Figure 2. Trajectory of a particle confined in a cylindrical vessel.

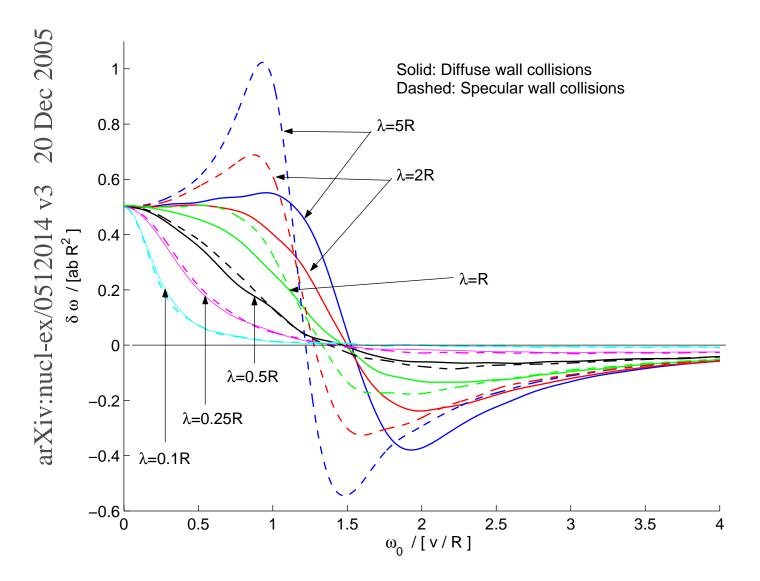
appropriate.  $r_o = R/\lambda = 50, 10.$ model equation (11), green - short mean free path limit equation (14) where tions and from the analytic model. red - numerical simulation, blue - complete Figure 3a. Comparison of correlation function,  $R(\tau)$  from numerical simula-

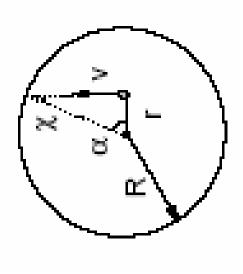
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Figure 3b) As figure 3a) r_o = 0.5, 1, 2.5, 6, 7.5
Figure 3c. Dependence of k = \lambda(T)/R on temperature.
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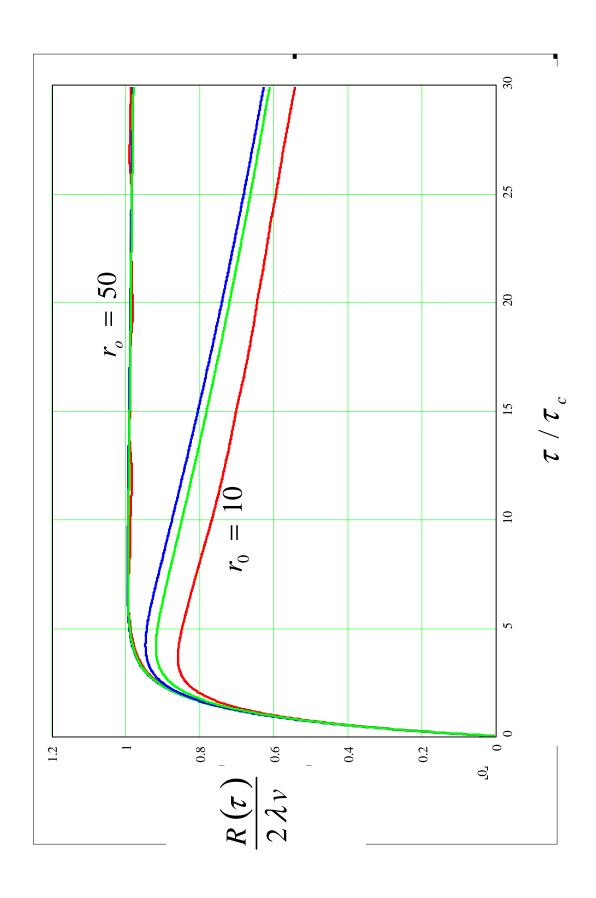
Figure 4. Normalized, velocity averaged fequency shift vs. normalized frequency:  $X(\omega,T)=\omega R/\beta$  (T). red T=0.3K, blue 0.35K, green 0.4K, purple 0,45K

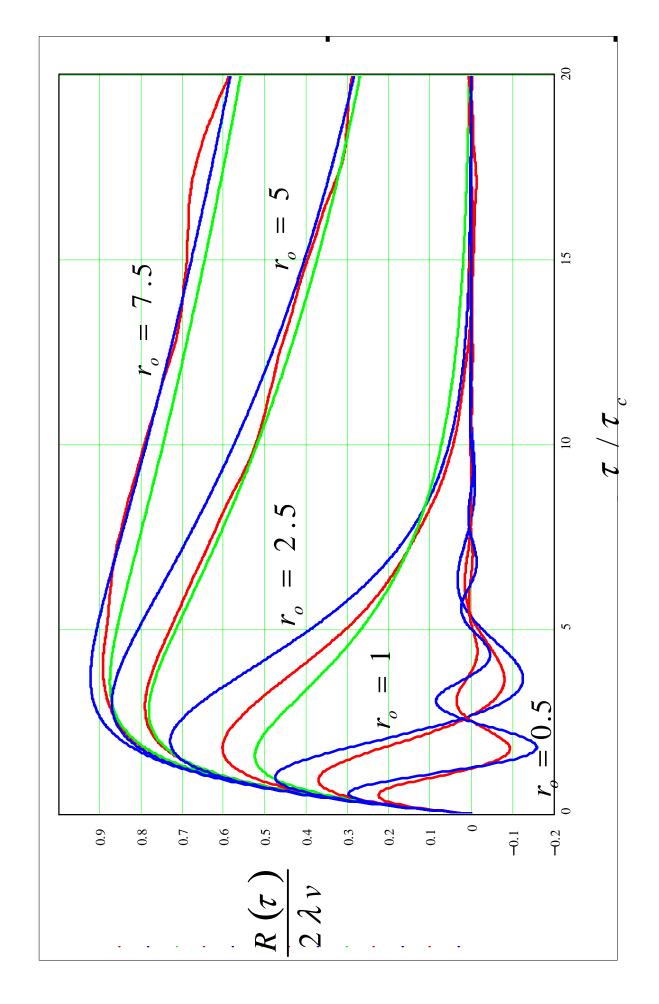
quency, expanded scale. red T=0.3K, blue 0.35K, green 0.4K, purple 0,45K Figure 5. Normalized, velocity averaged fequency shift vs. normalized fre-

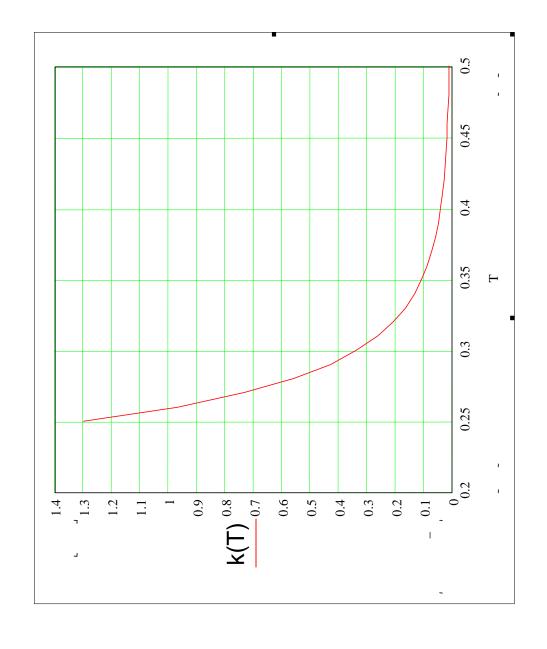
- Figure 6. Normalized, velocity averaged fequency shift vs. normalized frequency. Same as figure 8, but expanded further. red T=0.3K, blue 0.35K, green 0.4K, purple 0,45K
- for various frequencies., red X=1.4, blue X=1.5, green X=1.7, purple X=1.8Figure 7. Velocity averaged frequency shift as a function of temperature, K,
- interesting region, red X=1.4, blue X=1.5, green X=1.6, purple X=1.7, light K, for various frequencies. As figure 7, scale expanded to show experimetnally Figure 8. Velocity averaged frequency shift as a function of temperature,
- is the normalized frequency,  $X = \omega R/\beta(T)$  with  $\beta(T)$  the most probable  $He^3$ velocity dependence of the  $He^3$  mean free path, for various temperatures. X velocity. green T=0.35K, purple T=0.38K, red T=0.4K, blue T=0.43K. Figure 9. Frequency shift averaged over velocity distribution, allowing for
- velocity dependence of the  $He^3$  mean free path, versus temperature, K, for various frequencies specified by the value of  $X = \omega R/\beta$  with  $\beta$  the most probable  $He^3$  velocity. blue X=3, green X=2.2, red X=2, purple X=1.8. Figure 10. Frequency shift averaged over velocity distribution, allowing for
- Figure 11. Expanded plot of the frequency shift averaged over velocity distribution, allowing for velocity dependence of the  $He^3$  mean free path, versus temperature, K, for various frequencies specified by the value of  $X = \omega R/\beta(T)$  with  $\beta(T)$  the most probable  $He^3$  velocity. blue X=3, green X=2.2, red X=2, purple X=1.8.

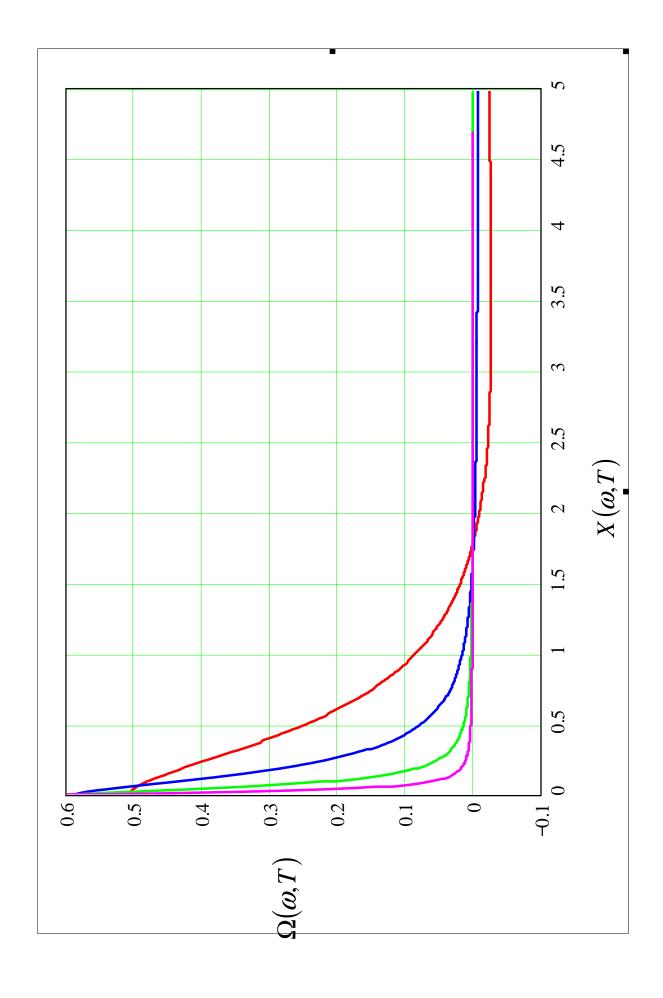


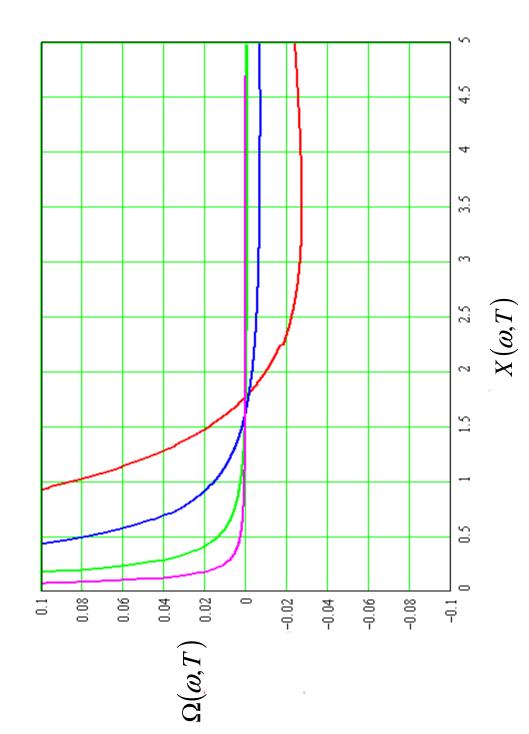


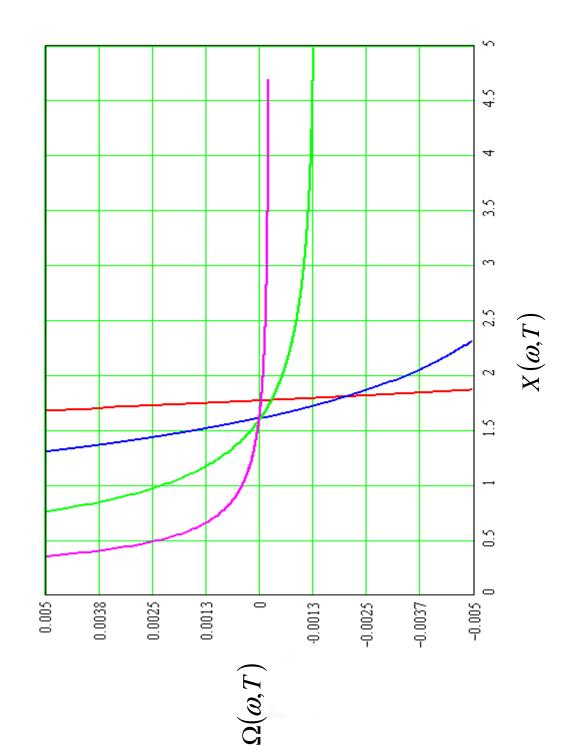


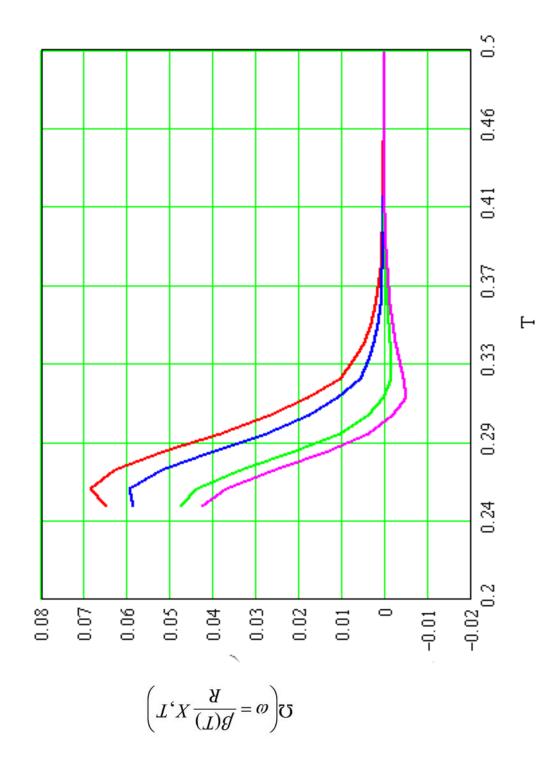


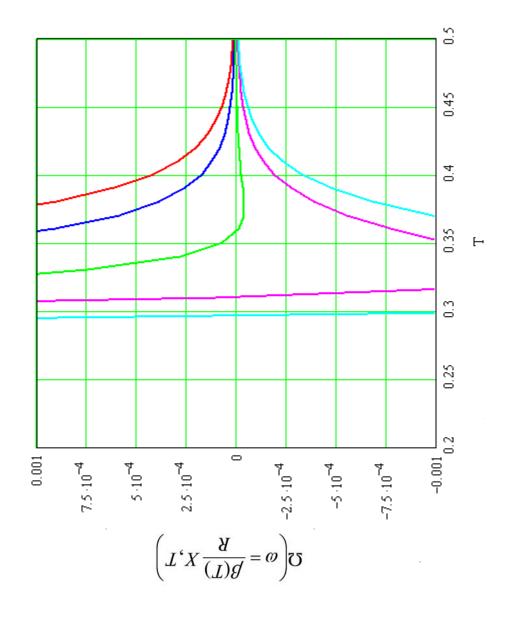


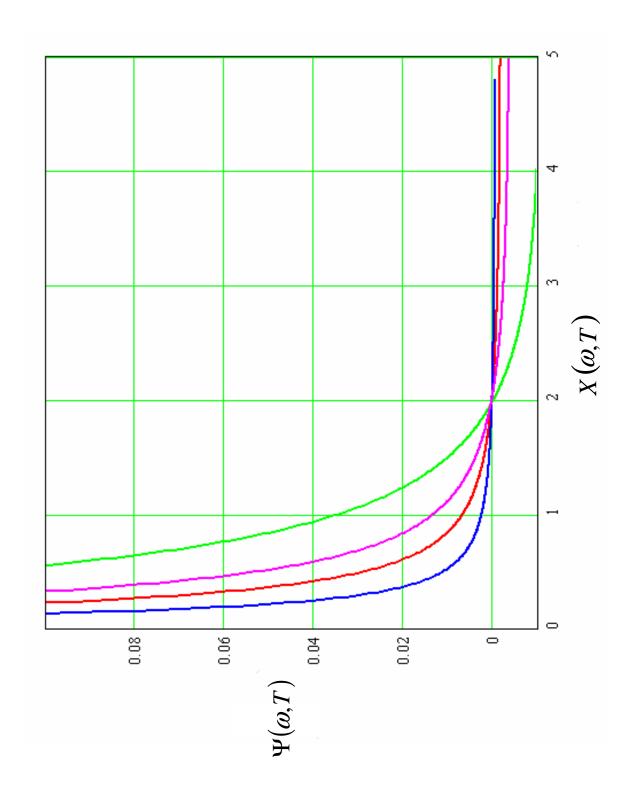


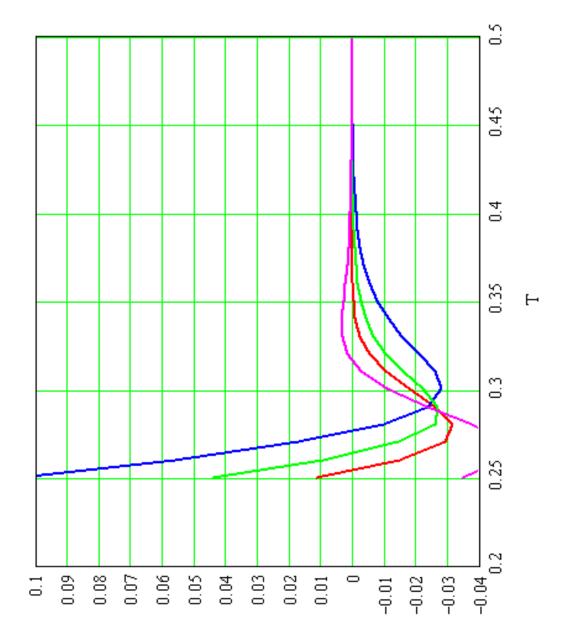












$$\int_{\mathbb{R}^{n}} \left( L'X \frac{\mathcal{Y}}{(L)\mathcal{G}} = \omega \right) dA$$

